

AS 4055:2021 AS 1684.2:2021

Wind Assessment for Residential Projects (Part 2)





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Link to the previous webinars: https://www.youtube.com/@ClearCalcs



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Meet the Presenters

- Qiming Liu, Structural Engineer
 - PhD in Structural Engineering
 - PhD from Swinburne University of Technology
 - MSc and BEng in Civil Engineering
 - 4 years of academic research experience in:
 - Topology Optimisation
 - 1 year now with ClearCalcs
 - Content Development
 - Customer Success





How to Ask Questions

Meeting Chat

• Type your questions in the Chat tab on your Zoom control panel and click Send

- Please send your questions to "everyone"
- We will address all questions in the second half of the webinar during the 15-minute Q&A session
- We might invite you to unmute yourself to ask your question live!





Agenda – Today's Goals

- Overview of AS 4055 and AS1684.2
 - Scope and limitation

• Wind Bracing for Residential Houses

- Definitions and design procedure
- Wind classification and racking force
- Design bracing systems

• Worked Examples

• Using ClearCalcs Wind Bracing Calculator



Overview of AS 4055 and AS 1684.2

- AS 4055 vs AS1170.2
- AS 1684.2

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AS 4055:2021

•AS 4055 "Wind Loads for Housing", a simplified version of AS 1170.2.

Scope: NCC Class 1 and 10a buildings with geometric limits.

•Simplifying assumptions and results in simple table lookup.

•Simplified coefficients & factors.

•Total Uplift/Racking – independent section with its own table lookups.





3.1 PRESSURE ZONES ON HOUSING-ROOFS (PLAN VIEW)



Table

Topogra

T1

NS

N2

N2

N3

N3

N3

N3

N4







AS 1684.2:2021

•AS 1684.1, Design Criteria (AS 1720.3 – Timber structures design criteria for timber-framed residential buildings)

•AS 1684.2, Prescriptive Non-cyclonic areas

•AS 1684.3, Prescriptive Cyclonic areas

•AS 1684.4, Simplified part 2

•Class 1 or 10a buildings, Single or two-storey construction.

•Building shapes: shall be essentially rectangular, square, L-shape or a combination of rectangular elements including splayed-end and boomerang-shaped buildings.

•Geometric limits:

- Max width: 16 m
- Max roof pitch: 35 deg
- Max wall height: 3.0 m (** 3.6m)

Wind Classification applicable to AS 4055
Spacing of bracing walls:

- 9.0 m max (ceiling diaphragm)
- 14.0 m max (floor diaphragm)





Wind Bracing of Residential Houses

Definitions and design procedure Wind classification and racking force Design bracing systems

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Bracing in AS 1684.2

- •Cl 6.1.3: "**Temporary and permanent bracing** shall be provided to stud walls to resist horizontal forces applied to the building."
- •Cl 8.1: "**Permanent bracing** shall be provided to enable the roof, wall and floor framework to resist horizontal forces applied to the building (racking forces). Appropriate **connection** shall also be provided to transfer these forces through the framework and subfloor structure to the building's foundation."
- •Temporary bracing shall be equivalent to at least 60% of the permanent bracing required.
- •Temporary bracing may from part of the installed permanent bracing.



28 June 2023



Bracing in AS 1684.2

Load Path





Bracing in AS 1684.2

Cl 8.3.1 – Wall and Subfloor Bracing

(a) Determine wind classification – Cl 1,5, or (AS 4055 or AS 1170.2 applicable)

(b) Determine the wind pressure – CI 8.3.2, or (AS 4055 or AS 1170.2 applicable)

(c) Determine the area of elevation – CI 8.3.3, Fig 8.2(A-C), or CI 5.2 of AS 4055

(d) Calculate the racking force - Cl 8.3.4,

(e) Design bracing systems for: (i) subfloors – Cl 8.3.5

(ii) walls - Cl 8.3.6

(f) Check even distribution and spacing – Cl 8.3.6.6, 8.3.6.7, Table 8.20 and Table 8.21

(g) Check connection of bracing to roof/ceiling and floors - Cl 8.3.6.9 and 8.3.6.10



AS 4440-2004

Australian Standard[™]

trusses

Installation of nailplated timber roof

Bracing in AS 1684.2

Cl 8.3.7 – Roof Bracing

- Cl 8.3.7.1 Pitched Roofs and Cl 8.3.7.2 Gable Roofs:
- Provides specifications and basic requirements only
- Diagonal metal bracing/sheet bracings to be designed and installed in accordance with engineering principles.
- Cl 8.3.7.3 Trussed Roofs
- In accordance with AS 4440 installation of nail plated timber roof trusses



4440



Step (a) Determine wind classification

Determine Wind Classification

CI 1.4.2, AS 1684.2:2021

1.4.2 Wind classification

For wind loads, the simplified wind classifications for non-cyclonic areas N1 to N4, as described by AS 4055, shall be used with the corresponding maximum design gust wind speeds given in <u>Table 1.1</u>.

Either AS 4055 or AS/NZS 1170.2 shall be used to determine the wind classification necessary for the use of this Standard.

The wind classifications covered by this Standard shall be determined as follows:

- (a) Where the wind classification is determined from AS 4055, the maximum building height limitation of 8.5 m, as given in AS 4055, shall apply to this Standard. The maximum building width is specified in <u>Clause 1.4.5</u>.
- (b) Where AS/NZS 1170.2 is used to determine the maximum design gust wind speed, a wind classification shall be adopted in accordance with <u>Table 1.1</u>. The ultimate limit state design gust wind speed determined from AS/NZS 1170.2 shall be not more than 5 % greater than the ultimate limit state wind speed given in <u>Table 1.1</u> for the corresponding wind classification adopted.

NOTE 1 The determination of the design gust wind speed and wind classification should take into account the building height, terrain category, topographic classification and shielding classification given in AS/NZS 1170.2 or AS 4055.

NOTE 2 Some relevant authorities provide wind classification maps or wind classifications for designated sites within their jurisdiction.





Step (a) Determine wind classification

Determine Wind Classification

♦ AS 4055:2021

Roof pitch 35° max. **Roof pitch** 35° max. 8.5 mb One or 8.5 m^b two storey One or 6.0 m^a 6.0 mª two storey ≤ 3 m Max 3 m 16.0 m max 16.0 m max. Roof pitch 35° max. Height at any section through the house 8.5 m max. 6.0 m^a 16.0 m max. AS 4055, fig 1.2 (a) Sections W $L \leq 5W$ 16.0 m max. -----16.0 m max. _____

- Geometric Limitations:
- $\circ \quad W \leq 16m$
- o $L \leq 5W$
- $\circ \ H \leq 8.5 \ m$
- $\circ h \leq 6m$
- o $\alpha \leq 35^{\circ}$

Edge of eaves

W 16.0 m max.

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Step (a) Determine wind classification

Determine Wind Classification

AS 4055:2021

- Design gust wind speed and wind classification assessment
- o Cl 2.2 Wind Region (A, B, C & D)
- o Cl 2.3 Terrain Category (1, 2, 2.5 & 3)
- o Cl 2.4 Topographic Classification (T0-T5)
- o Cl 2.5 Shielding Classification (FS, PS, NS)

Table 2.2 — Site wind classification from wind region and site conditions

							Topog	aphic classi	fication					
Wind	тс	Т0	то	TO	T1	T1	T1	T2	T2	T2	Т3	T3	T4	T5
region		FS	PS	NS	FS	PS	NS	FS	PS	NS	PS	NS	NS	NS
	3	N1	N1	N1	N1	N2	N2	N2	N2	N2	N3	N3	N3	N4
	2.5	N1	N1	N2	N1	N2	N2	N2	N3	N3	N3	N3	N4	N4
A	2	N1	N2	N2	N2	N2	N3	N2	N3	N3	N3	N3	N4	N4
	1	N2	N2	N3	N2	N3	N3	N3	N3	N3	N4	N4	N4	N5
	3	N2	N2	N3	N2	N3	N3	N3	N3	N4	N4	N4	N4	N5
	2.5	N2	N3	N3	N3	N3	N3	N3	N4	N4	N4	N4	N5	N5
в	2	N2	N3	N3	N3	N3	N4	N3	N4	N4	N4	N5	N5	N6
	1	N3	N3	N4	N3	N4	N4	N4	N4	N5	N5	N5	N6	N6
	3	C1 (0-50)	C2 (0-10) C1 (10-50)	C2 (0-20) C1 (20-50)	C2 (0-5) C1 (5-50)	C2 (0-30) C1 (30-50)	C2 (0-40) C1 (40-50)	C2 (0-25) C1 (25-50)	C3 (0-5) C2 (5-50)	C3 (0-20) C2 (20-50)	C3 (0-25) C2 (25-50)	C3 (0-30) C2 (30-50)	C4 (0-10) C3 (10-50)	C4 (0-35) C3 (35-50)
	2.5	C1 (0-50)	C2 (0-25) C1 (25-50)	C2 (0-35) C1 (35-50)	C2 (0-20) C1 (20-50)	C2 (0-40) C1 (40-50)	C3 (0-10) C2 (10-50)	C2 (0-35) C1 (35-50)	C3 (0-20) C2 (20-50)	C3 (0-30) C2 (30-50)	C3 (0-35) C2 (35-50)	C4 (0-5) C3 (5-50)	C4 (0-25) C3 (25-50)	NA (0-15) C4 (15-50)
	2	C2 (0-10) C1 (10-50)	C2 (0-35) C1 (35-50)	C2 (0-45) C1 (45-50)	C2 (0-30) C1 (30-50)	C3 (0-10) C2 (10-50)	C3 (0-25) C2 (25-50)	C3 (0-10) C2 (10-50)	C3 (0-30) C2 (30-50)	C3 (0-40) C2 (40-50)	C4 (0-10) C3 (10-50)	C4 (0-20) C3 (20-50)	NA (0-5) C4 (5-50)	NA (0-25) C4 (25-50)
	1	C2 (0-30) C1 (30-50)	C3 (0-10) C2 (10-50)	C3 (0-25) C2 (25-50)	C3 (0-10) C2 (10-50)	C3 (0-30) C2 (30-50)	C4 (0-5) C3 (5-50)	C3 (0-25) C2 (25-50)	C4 (0-10) C3 (10-50)	C4 (0-20) C3 (20-50)	C4 (0-30) C3 (30-50)	NA (0-5) C4 (5-50)	NA (0-25) C4 (25-50)	NA (0-45) C4 (45-50)

AS 4055, table 2.2 - D is on the 2^{nd} part of this table

Determine the Racking Force

Racking force

- CI 5.1 of AS 4055 and CI 8.3.4 of AS 1684.2
- Total racking force = Area of elevation (m 2) × Lateral wind pressure (kPa).

Area of Elevation

- CI 5.2 of AS 4055, and CI 8.3.3 of AS 1684.2
- Should be calculated for both directions (long & short sides) of the building
- "The wind direction used shall be that resulting in the greatest load for the length and width of the building, respectively. As wind can blow from any direction, the elevation used shall be that for the worst direction."







(a) Plan





(c) Wind direction 2

AS 4055, fig 5.2(A)



Step (b) Determine wind pressure

Determine the Racking Force

Total racking force = Area of elevation (m 2) × Lateral wind pressure (kPa).

- Determine the Wind Pressure
- Surface type:
 - Vertical Surfaces
 - o Table 5.2(A) of AS 4055, Table 8.1 of AS 1684.2
 - Sloped Roofs

(hip roofs or side wind on gable/skillion roofs)

• Table 5.2 (B-M) and Table 8.2-8.5 of AS 1684.2





Step (b) Determine wind pressure and step & (d) Calculate the racking force

Determine the Racking Force

Total racking force = Area of elevation (m 2) × Lateral wind pressure (kPa).

Determine the Wind Pressure

Wind Class, Roof pitch (α) and Width of the building (W ٠



	Single st	torey or up	per floor of	two storeys	- 2.4 m st	orey, 0.3 m	floor				
Width (m) Roof pitch (degrees) 0 5 10 15 20 25 30 20											
(m)	0	5	10	15	20	25	30	35			
			5		$\langle \rangle$						
						H					
		Wind directi	on	Wind	direction	W					
1: Wind on s	ide										
4	0.58	0.51	0.46	0.43	0.47	0.53	0.53	0.54			
5	0.58	0.49	0.44	0.42	0.47	0.53	0.52	0.54			
6	0.58	0.48	0.41	0.42	0.48	0.53	0.52	0.55			
7	0.58	0.46	0.39	0.42	0.48	0.53	0.52	0.55			
8	0.58	0.45	0.37	0.42	0.48	0.53	0.52	0.55			
9	0.58	0.44	0.35	0.42	0.49	0.53	0.52	0.55			
10	0.58	0.43	0.33	0.41	0.49	0.53	0.52	0.55			
11	0.58	0.41	0.32	0.41	0.48	0.53	0.52	0.55			
12	0.58	0.40	0.31	0.40	0.48	0.52	0.52	0.55			
13	0.58	0.39	0.30	0.39	0.48	0.52	0.51	0.55			
14	0.58	0.38	0.29	0.39	0.47	0.52	0.51	0.55			
15	0.58	0.38	0.28	0.38	0.47	0.52	0.51	0.55			
16	0.58	0.37	0.27	0.38	0.47	0.51	0.51	0.55			
		~		~							
		$rac{1}{2}$		Day	2						
			12		1						
		V.	WWW	nd direction	WWin	d direction					
1: Wind on e	nd		7		7						
4	0.63	0.59	0.56	0.54	0.55	0.57	0.56	0.57			
5	0.63	0.58	0.54	0.52	0.55	0.57	0.56	0.57			
6	0.63	0.57	0.52	0.52	0.55	0.56	0.55	0.57			
7	0.63	0.56	0.51	0.51	0.55	0.56	0.55	0.57			

0.63

0.55

0.49

0.51

0.55

0.56

0.55

0.57

Table 5 2(B) — Hip roofs and side wind on gable roofs — Prossure (kPa) on area of elevation

S 4055, Table 5.2(B)

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Bracing Systems

Nominal Wall Bracing – Cl 8.3.6.2

- "the racking force is resisted by a combination of "Structural Wall Bracings" and also "Nominal Wall Bracings"..."
- Internal linings of the building (e.g. gyprock, villaboard)
- The maximum allowance for nominal bracing is 50% (both direction)
- Nominal bracing should be evenly distributed throughout the family and the second state of the second st
- Minimum length for nominal bracing is 450mm

Structural Wall Bracing - Cl 8.3.6.3

- Purpose-fitted bracing
- Sheet or cross-timber or steel bracing
- 14 commonly used bracing types are provided

in Table 8.18 (type a, b, c, ..., n)

Method	Bracing Capacity (kN/m)
Sheeted one side only	0.45
Sheeted two sides	0.75

AS 1684.2, Table 8.17





Bracing Systems

Metal or Timber Diagonal Bracings

- Type (a)-(d), Maximum capacity of 3.0 kN/m, Maximum Wall height: 2700mm,
- Wall length: 1800 mm Min. to 2700 mm Max.
- Fixed bottom plate to floor frame or slab with nominal fixing only (Table 9.4)

Туре	Description	Material and thickness (mm)	Capacity, (kN/m)	Requirements
(a)	Two diagonally opposed timber or metal angle braces	Timber: 45x19 or 70x19 hardwood, Steel: 18x16x1.2	0.8	
(b)	Metal straps – tensioned		1.5	
(c)	Timber & metal angle braces	Timber: 75x15 F8 or Steel: 20x18x1.2	1.5	Length: 1800 mm min. to 2700 mm max
(d)	Metal straps – tensioned – with stud straps		3.0	

Table 8.18(c) — Structural wall bracing (maximum wall height 2.7 m)



AS 1684.2, Table 8.18(c)

AS 1684.2: 2021, Table 8.18 (a)-(d)



Bracing Systems

Plywood Sheet Bracings, type (g)-(k):

- Maximum wall height: 2700 mm
- Capacities are JD5, which reduced from 2010 version (JD4)
- Minimum length of (g)-(i) is 900 mm, except Method A of (h) 600mm
- Detail (g) half (1.5 kN/m) for unit length 600mm

Туре	Brief Description	Capacity (kN/m)	Requirement Length (mm)
(g)	Plywood, various grade and thicknesses	3.0	900
(h)	Plywood, various grade and thicknesses Method A	5.6	600
	Plywood, various grade and thicknesses Method B	5.2	900
(i)	Plywood, 4.5mm F11	6.6	600
	Plywood, 7 mm F11	7.6	600
(j)	Plywood, F11 (decorative)	1.8	900
(k)	Plywood, F11 (decorative)	4.6	900



AS 1684.2, Table 8.18(q)

AS 1684.2: 2021, Table 8.18 (g)-(k)



Bracing Systems

Hardboard Sheet Bracings

- Not so commonly available
- Capacities are JD5, which reduced from 2010 version (JD4)
- Maximum wall height: 2700 mm
- Minimum thickness of hardboard: 4.8 mm
- One-side of the wall to be lined with plasterboard or equivalent

Туре	Brief Description	Capacity (kN/m)	Requirement Length (mm)
(1)	Hardboard, Type A	2.9	900
(m)	Hardboard, Type B	5.0	900
	Hardboard, Type C	7.6	900
(n)	Hardboard, Type D	2.9	460
	Hardboard, Type E	5.0	460



NOTE Bolt/rod washer sizes are set out in Table 9.1.

AS 1684.2, Table 8.18(n)

AS 1684.2: 2021, Table 8.18 (I)-(n)



Bracing Systems

Height Modification – Cl 8.3.6.4

- In Table 8.18 (a) (n), the wall heights is up to 2700 mm
- For walls greater than 2700mm, the capacity shall be reduced by multiplying by the height accordingly
- For example: Wall height of 3900 mm, 10m of plywood bracing type (g), 3.0 kN/m capacity

Bracing resistance provided: = 3.0 kN/m x 10 m x 2700/3900 = 20.77 kN (30 kN without reduction)

JD5 to JD4 framing – Cl 8.3.6.3

- In Table 8.18 (g) (n), based on minimum JD5 or J5
- Information of Joint Groups refer to Cl 9.6.5 and Appendix G
- If JD4 is used:

Plywood (g) – (k): increase capacity by 12.5%Hardboard (l) – (n): increase capacity by 16.0%

Alternate Bracings:

e.g. Portal Frames (Cl 8.3.6.7) and Masonry Walls (Cl 8.3.6.8), OSB Sheet Braces, Wall Trusses.

Refer to capacities provided by the manufacturers

Wall Height (mm)	Multiplier
3000	0.9
3300	0.8
3600	0.75
3900	0.7
4200	0.64

AS 1684.2, Table 8.19



Step (f) Check even distribution and spacings

Bracing Systems

Location and Distribution – CI 8.3.6.6

"Bracing shall be approximately evenly distributed and provided in both directions, and shall initially be placed in external walls and if possible, at corners of the building"



Step (f) Check even distribution and spacings

Bracing Systems

Spacing – CI 8.3.6.7 and CI 8.3.5.9

Wind Class N1 and N2	Spacing of Bracing						
Single or Upper Floor of two Storey Building	9,000 mm	9,000 mm					
Lower of Two Storey Building	9,000 mm						
	14,000 mm						
Wind Class N3 and N4	Spacing of B	Spacing of Bracing by Roof Pitch					
Single or Upper Floor of two Storey Building	Read from Table 8.20 and 8.21						
	9,000 mm						
Lower of Two Storey Building	Read from Table 8.20 and 8.21						
	14,000 mm						

Spacing betwe walls for wind o (Panels 5, 6 an Wing dire	en bracing direction B nd 7) 1 5 5 6 7 1 0 7	2 6 3 4	Spacing between bracing walls for wind direction A (Panels 1, 2, 3 and 4)



Step (g) Check Connections

Bracing Systems

Fixings of top of bracings – Cl 8.3.6.9

"All internal bracing walls shall be fixed to the floor of lower storey bracing walls, the ceiling or roof frame, and/or the external wall frame, with structural connections of equivalent shear capacity to the bracing capacity of that particular bracing wall."

"Nominal and other bracing walls with bracing capacity up to 1.5 kN/m require nominal fixing only, i.e. no additional fixing requirements.

Table 8.22 (a) to (i) outlines the requirements for the bracing wall to ceiling connections

Table 8.22(b) — Fixing of top of bracing walls





Step (g) Check Connections

Bracing Systems

Fixings of bottom of bracings – Cl 8.3.6.10 *

"The bottom plate of timber-framed bracing walls shall be fixed at the ends of the bracing panel and, if required, intermediately to the floor frame or concrete slab with connections determined from Table 8.18."

- Connections in Table 8.18 is for capacity up to 3.4 kN/m
- Otherwise, need to refer to Table 8.23 and Table 8.24

				decision for the										Γ				Uj	olift ca	pacity,	kN	
Table 8.23 — Uplift force at ends of bracing walls							,	Fixing details			season timber	ied	Seasoned timber									
Wall height,			1	Uplif For bra	t force acing v	e at eno walls r	is of b ated a	racing t (kN/i	walls, n) cap	KN acity					~~		J2	J3	J4	JD4	JD5	JD6
mm	1	1.5	2	2.5	3	3.5	4	4.5	5	5.5	6	8	10	'	(a) M10 cup-head bolts or No. 14 Type 17	M10 aug						
2 400	2.4	3.6	4.8	6.0	7.2	8.4	10	11	12	13	14	19	24	11	batten screws as per table, with min.	head	16	14	10	10	7	5
2 700	2.7	4.1	5.4	6.8	8.1	9.5	11	12	14	15	16	22	27		38 mm penetration into flooring and/or joist	2/No.14					5 5	
3 000	3.0	4.5	6.0	7.5	9.0	11	12	14	15	17	18	24	30			Type17	11	8.4	4.8	9.0	7.2	5.4
NOTE 1 So plate to the f NOTE 2 Th Supplements	OTE 1 Some bracing wall systems require fixings to be full-length anchor rods, i.e. from the top ate to the floor frame or concrete slab. OTE 2 The maximum tension load of 8.5 kN given in the Notes to Span Tables for studs in the pplements is not applicable when considering the uplift force at the ends of bracing walls.								screws	1	A.											
NOTE 3 W lieu of the de	here pi tails d	rovided, etermin	the b ed froi	ottom n <u>Table</u>	plate t es 8.23	ie-dow and <u>8.</u>	n deta <u>24</u> .	ils give	en in <mark>T</mark>	able 8.	. <u>18</u> ma	y be u	sed in									

Table 8.24(a) — Fixing of bottom of bracing walls

AS 1684.2, Table 8.23 and 8.24

ⓓ ClearCalcs

	*	Covered By ClearCalcs					
(a)	Determine wind classification					
(b)	(b) Determine the wind pressure					
	(c) D	Determine the area of elevation					
	(d) Calculate the racking force						
	(e) [Design bracing systems for: (i) subfloors					
		(ii) walls					
	(f) C	heck even distribution and spacing					
	(g) (Check connections					

Worked Examples

How does the workflow look like in ClearCalcs Wind Bracing Calculator

Objective Objective ClearCalcs

Worked Example

Design a simple wall bracing for a residential building

- Single storey rectangular house:
 - L = 16.2m, W = 7.2m, H=3.0m, Roof pitch = 20⁰
 - Wind Class on site: N2
- Nominal bracings (calculated on site):
- Long-side: two-sheeted 9.5 m
- Short-side: one-sheeted 5 m
- Design structural wall bracings:
- Long-side:
 - two diagonally opposed timber/metal angle braces, type (a)
 - Cycled bracing (metal bracing) with a unit capacity of 1.7 kN/m, 10m in total.
- Short-side:
 - plywood type braces, type (g)







Questions?





THANK YOU!

- We will send you a recording of the webinar by email.
- There will be a survey at the end of this webinar, we would appreciate your feedback on how we can improve.
- If you have further questions, send an email to <u>help@clearcalcs.com</u> or use the Help button in ClearCalcs
- Stay tuned for webinar [Webinar Title] next month!



Appendix

About ClearCalcs



Happy Engineers Using ClearCalcs

ClearCalcs has been used in 2,000,000+ designs by a growing number of engineers across the globe, with the US becoming our largest customer base in 2021.







"You are light years ahead of the competition on features and ongoing growth." "Why didn't you just use ClearCalcs for that?"

"The program basically does the work for you...Wow, I can finally throw away the last of my spreadsheets!"

Don C. Foundation Engineering Specialists, LLC

Helen W. via Landon R. Criterium Engineers **Jason M.** J. Michael Engineering, PLLC





The ClearCalcs Team

A growing team of passionate engineers, programmers, customer success specialists, product managers, marketers, and more!





What Sets Our Calculations Apart

• Live solutions

• Instantly see how every change you make affects the design, in all load cases

• Finite Element Analysis

• Get the most accurate results no matter what your configuration

• As simple or complex as you want

• Safely enter in only a few properties, or tune every parameter – it's up to you







What Sets Our Design Process Apart

Member selector

- Check every possible member in seconds
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Designation	M_d V_d δ_l δ_s
70 x 35 F5 Seasoned SW	450% 91% 417% 752%
90 x 35 F5 Seasoned SW	273% 71% 198% 354%
120 x 35 F5 Seasoned SW	154% 53% 84% 150%
140 x 35 F5 Seasoned SW	113% 46% 53% 95%
190 x 35 F5 Seasoned SW	62% 34% 22% 38%

Roof	Lintel RL8				÷
	Location G	overning Reactions F	ermanent Load Reactions	Imposed Load Reactions	
Support	Location G (mm)	verning Reactions F R* (kN)	ermanent Load Reactions R*_G (kN)	Imposed Load Reactions R*_Q (kN)	
Support 1	Location G (mm)	0.293	Permanent Load Reactions R*_G (kN) 0.0667	Imposed Load Reactions R*_Q (kN) 0.133	





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	· 1	ல	Client: Engineer: Brooks Smith Project: test	Date: Oct 17, 2018 Job #:			
erstand		Moment Demand about X-Axis $M_a^r = 10.3 \text{ kNm}$ 85% Moment Capacity about X-Axis $\phi M_a = 12.2 \text{ kNm} \Rightarrow M_{am}$ Shear Demand $V = 20.7 \text{ km}$ 18% Shear Capacity $\phi V_a = 118 \text{ km} \Rightarrow M_{am}$					
cistana		$\label{eq:starset} \begin{array}{ c c c } \hline Shear Capacity (AS4100-1998, Section 5.11) \\ \hline Shear Capacity Factor & \phi = 0.9 \\ \hline Nominal Shear Yield Capacity & V_{\phi} = 131 kN & e.t. f_{\mu_1, e.v., e.t., e.$					
Weak Axis Buckling Stress	$f_{oy}=~112~{ m MPa}$		Moment Section Capacity (AS4100-	1998, CI 5.3)			
Torsional Buckling Stress	$f_{oz}=~82.2{ m MPa}$		$\phi=0.9$ pacity $M_s=32.6$ k	$\mathbf{Nm} = f_{\mu I} \cdot Z_{e} \cdot \mu I^{-40}$			
AS4600-2005, Eqn 3.3.3.2(12) Conditions: $(default) \rightarrow \frac{GJ}{(Aro^2)} \cdot \left(1 + \frac{\pi^2 E}{(GJ4_c}\right)$ Flexural-Torsional Factor	$\beta = 0.556$			Calcs			
s			What's New -	Improved			
		connections, diagrams, and more! New year, stacks of new ClearCalcs updates! We're excited to kick off 2019 with a bang with a bevy of new and imminent updates including new calculation templates and features.					
		Log	<u>in now</u> and have a look, or rea	d below to find out more.			
		Envelope	diagrams	a as (3/2/01/1995) a as (3/2/01/1995)			
		It's now easie the shear, mo	r than ever to graphically discer ment, and deflection forces act th all diagrams undated to a full	m I al I a			



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